

Nov 15



RF Amplifier

Including: Basic Modulator Alignment

D1340-aQ110-7

Instruction Manual

RFA1110-2-x Series

Models -

RFA1110-2 : 90-130MHz, dual output amplifier, 8W per output

Options -x:

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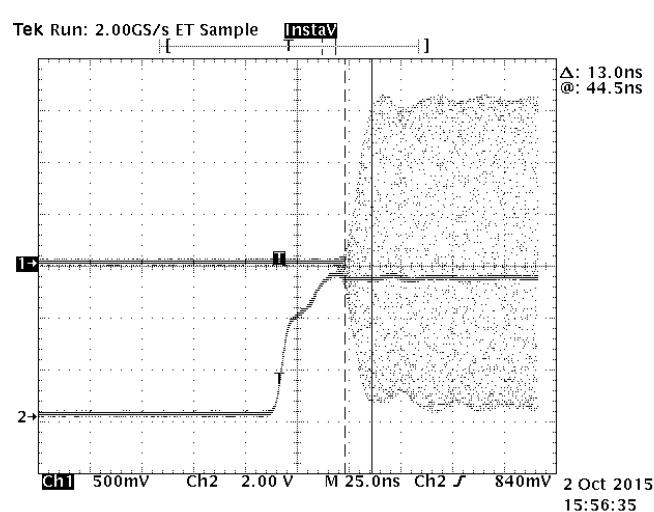
1. GENERAL

The RFA1110-2 Power Amplifier, figure 1, is a dual output broadband RF amplifier specifically designed to operate with Isomet acousto-optic devices such as the D1340-aQ110 series. The driver requires a low level signal from a suitable frequency source such as the Isomet iSA-SF1 frequency synthesizer. Figure 2 is a functional block diagram of the driver. A frequency input is required from an external source. A single turn potentiometer provides gain control for adjusting the maximum r-f power at the driver outputs. An RF mixer provides high speed amplitude modulation and a solid state switch provides an interlock function. The rise and fall response time for the amplifier is approx' 25nsec.

This amplifier is designed to operate at full rated power into a 50Ω load with 100% duty cycle.

Trace 1 = RF output

Trace 2 = modulation input



Water cooling is mandatory. The heatsink temperature must not exceed 70°C.

SERIOUS DAMAGE TO THE AMPLIFIER MAY RESULT IF THE TEMPERATURE EXCEEDS 70°C.

SERIOUS DAMAGE TO THE AMPLIFIER MAY ALSO RESULT IF THE RF OUTPUT CONNECTOR IS OPERATED OPEN-CIRCUITED OR SHORT-CIRCUITED.

A low impedance d-c power source is required. The operating voltage is +24V or +28Vdc at a current drain of approximately 3A (4A maximum). The external power source should be regulated to $\pm 2\%$ and the power supply ripple voltage should be less than 200mV for best results.

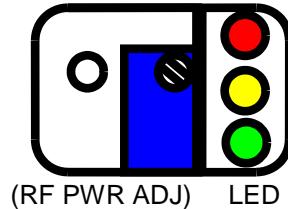
Higher RF output power is achieved at 28Vdc.

The output power level is set by the power adjust potentiometer (PWR ADJ)

Maximum power = fully clockwise

2.1 LED INDICATOR

The front panel tri-colour LED indicates the operating state.



RED

The top LED will illuminate RED when 24Vdc supply is applied.

Normal condition is ON

YELLOW

The middle LED will illuminate YELLOW, when the RF Gate input is valid.

(Default condition = valid, unless a connection is made to pin7 of the D-type)

Normal condition is ON, but may be OFF if the above conditions are not met

GREEN

The lower LED will illuminate GREEN when the following signals are all true:

- 1) RF DC power is applied and
- 2) Gate signal is valid and
- 3) Amplifier and AO thermal interlocks are valid *.

Normal condition is ON

* Thermal Interlocks

The AOM and Driver are fitted with thermostatic switches which will switch open circuit if a predetermined temperature is exceeded. These thermal interlocks will reset once the AO device and / or RF driver are cooled below this temperature.

- The driver thermal switch over-temperature threshold is 50deg C
- The AOD thermal switch over-temperature threshold is 36deg C

The hysteresis of the thermal switches is 7-10deg C.

Once in a fault state the coolant temperature will need to be reduced to reset the thermal switches.

3.0 INSTALLATION AND ADJUSTMENT

3.1 Connect cooling water at a flow of more than 1 litres/minute at < 20 deg.C to both the RF amplifier and AO device. Due to the RF power dissipated in the AO modulator, it is paramount that the device is operated only when water cooling is circulating. For optimum AO performance, ensure the flow rate is greater than 1 litre /minute at < 20 deg.C.

3.2 With no d-c power applied, connect the + 24V (or +28V) DC in to the screw terminal.
DO NOT APPLY POWER.

3.3 Connect the RF output BNC jacks to the acousto-optic deflector
(or a 50Ω RF load, if it is desired to measure the modulator RF output power).

Connection order depend on the Bragg orientation as shown on page 12.

3.3a Connect the RF input SMA jack to an external frequency source
(90 – 130MHz, 1mW max, 50Ω).
Set input power to 1 mW.

3.4 Connect the Interlock of the acousto-optic device to the mating connector of the RF driver
(Binder 3pin snap connector).

The interlock connection becomes open circuit disabling the RF output, if the temperature of the modulator exceeds 36°C or the internal driver temperature exceeds 50°C. The LED indicator illuminates when the Interlocks are closed and the RF is enabled (see Section 2).

- 3.5 Adjustment of the RF output power is best done with amplifier connected to the acousto-optic modulator. The Amplifier maximum output power is factory preset to approx 7W.

The optimum RF power level required for the modulator to produce maximum first order intensity will be different at various laser wavelengths. Applying RF power in excess of this optimum level will cause a decrease in first order intensity (a false indication of insufficient RF power) and makes accurate Bragg alignment difficult. It is therefore recommended that initial alignment be performed at a low RF power level.

- 3.6 Locate the PWR ADJ access on the driver end plate.

Note: Power adjustment range is approximately 6:1 e.g. 1.5 – 8W

- 3.7 With an insulated alignment tool or screwdriver rotate the PWR ADJ potentiometer fully anti-clockwise (CCW), then clockwise (CW) approx 1/4 turn.

- 3.8 Apply DC to the amplifier.

- 3.9 Apply a 1mW (0dBm) constant input to the input SMA connector of the RFA1110-2.

Input the laser beam toward the centre of either aperture of the AO device. Ensure the polarization is vertical with respect to the base and the beam height does not exceed the active aperture height of the AOM/AOD.

Start with the laser beam normal to the input optical face of the AOD and very slowly rotate the AOD (see page 12 for configurations.)

- 3.10 Observe the diffracted first-order output from the acousto-optic modulator and the undeflected zeroth order beam. Adjust the Bragg angle (rotate the modulator) to maximise first order beam intensity.

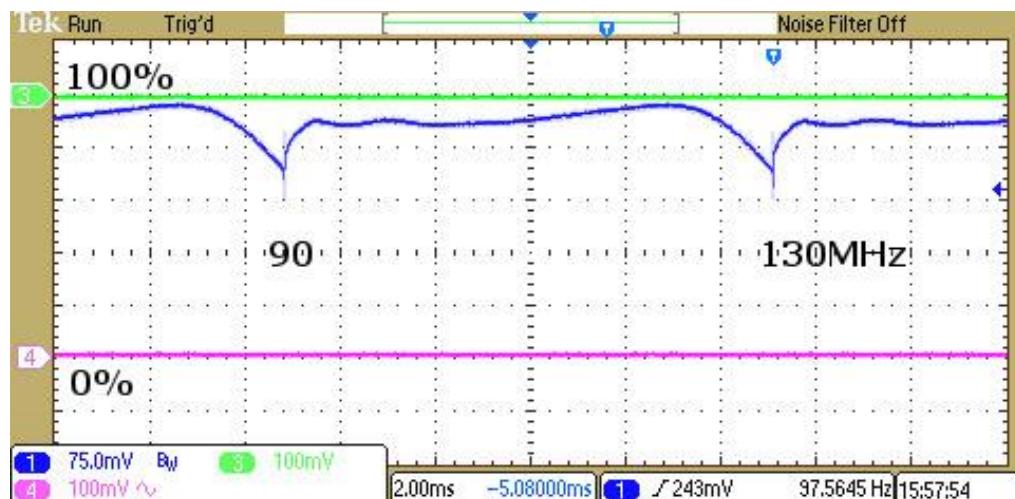
- 3.11 After Bragg angle has been optimized, slowly increase the RF power (rotate PWR ADJ CW) until maximum first order intensity is obtained.

- 3.12 To equalise deflection efficiency at the extremes of the scan, alternate between the minimum and maximum desired frequencies and adjust Bragg angle to give the same efficiency for both. (Note: the photo detector or light power meter will require repositioning for the two angles.) Sweeping the freq' input should result in a continuous deflected line output. If significant peaks and troughs are noted across the sweep, it is probable that the phase delayed output of the RF driver is connected to the incorrect input of the AO deflector.

The lead lengths between the two outputs of the RF driver and the beam steered deflector should be equal unless otherwise instructed. Unequal lengths of more than a 1cm would introduce a phase error.

Within limits, small changes in the relative lead lengths can be used to fine tune the deflector sweep response, although this is not usually required. The Bragg angle would need re-adjustment.

Typical swept frequency response at 374nm



First order diffraction efficiency vs RF drive frequency



4. MAINTENANCE

4.1 Cleaning

It is of utmost importance that the optical apertures of the deflector optical head be kept clean and free of contamination. When the device is not in use, the apertures may be protected by a covering of masking tape. When in use, frequently clean the apertures with a pressurized jet of filtered, dry air.

It will probably be necessary in time to wipe the coated window surfaces of atmospherically deposited films. Although the coatings are hard and durable, care must be taken to avoid gouging of the surface and leaving residues. It is suggested that the coatings be wiped with a soft ball of brushed (short fibres removed) cotton, slightly moistened with clean alcohol. Before the alcohol has had time to dry on the surface, wipe again with dry cotton in a smooth, continuous stroke. Examine the surface for residue and, if necessary, repeat the cleaning.

4.2 Troubleshooting

No troubleshooting procedures are proposed other than a check of alignment and operating procedure. If difficulties arise, take note of the symptoms and contact the manufacturer.

4.3 Repairs

In the event of deflector malfunction, discontinue operation and immediately contact the manufacturer or his representative. Due to the high sensitive of tuning procedures and the possible damage which may result, no user repairs are allowed. Evidence that an attempt has been made to open the optical head will void the manufacturer's warranty.

RFA 1110-2 Standard Version

Connection Summary

1.0 'D' Type Control Connection

<u>Signal</u>	<u>Type</u>	<u>Pin out connection</u>
Analogue Modulation < 0.4V(off) to 10.0V(on)	Input	Signal pin 8 Return pin 3
Digital Gate CMOS high (12V logic) or NC = ON CMOS low (0.0V < v < 1V) = OFF	Input	Signal pin 7 Return pin 2

2.0 Coaxial SMA

Low level RF Input

Frequency range	100 – 120MHz Typical 90 – 130MHz Maximum
Power level	0dBm (1mW) Typical 3dBm (2mW) Maximum

3.0 Interlock connection

AOM Thermal Interlock Plug
(OK = connected contacts
1-2)

RF Driver INT Plug
(OK = connected
contacts 1-2)



The interlock signal must be connected. Contacts closed for normal operation.

4.0 Mounting Holes

4 x M5

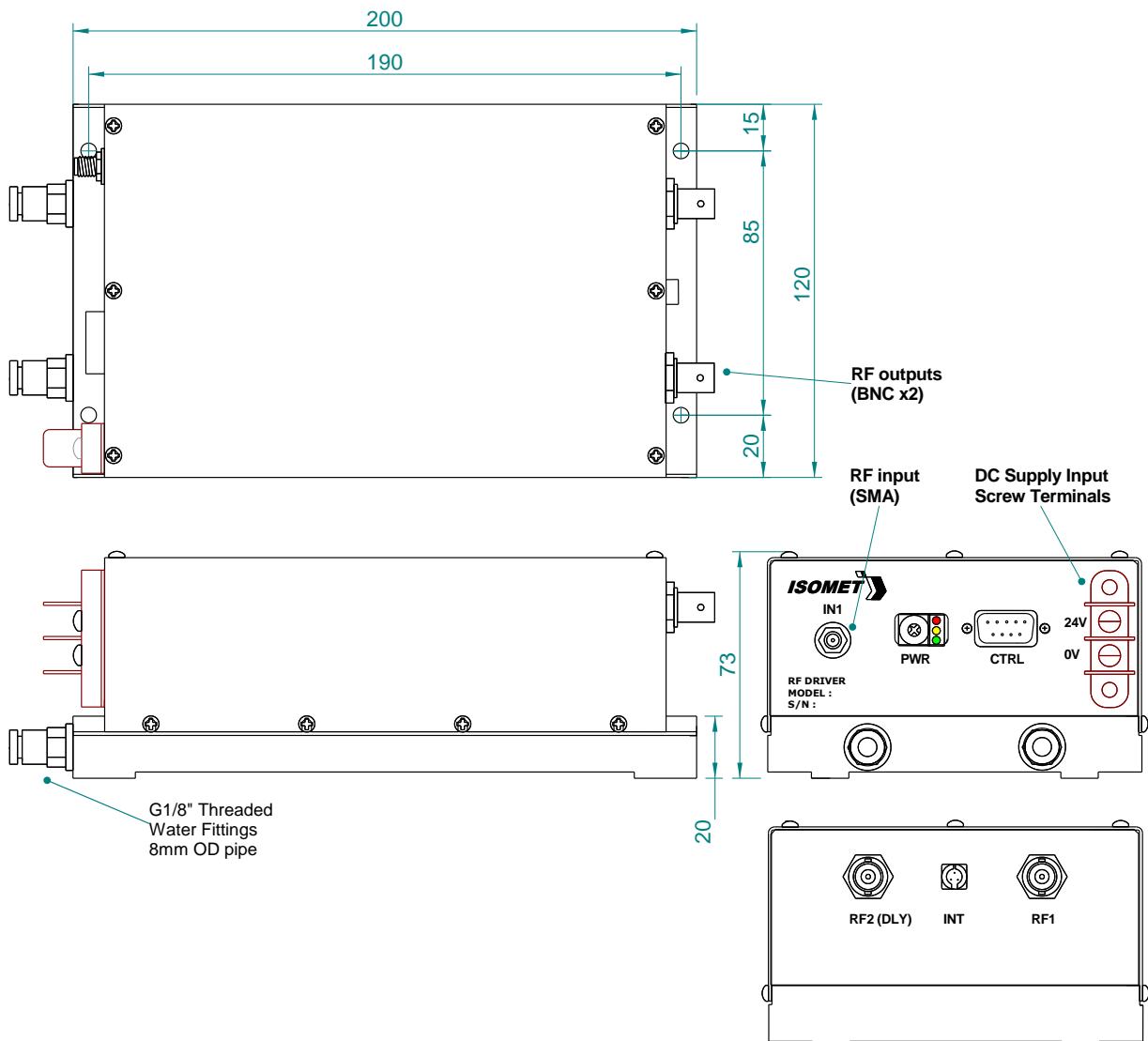


Figure 1: Driver Installation

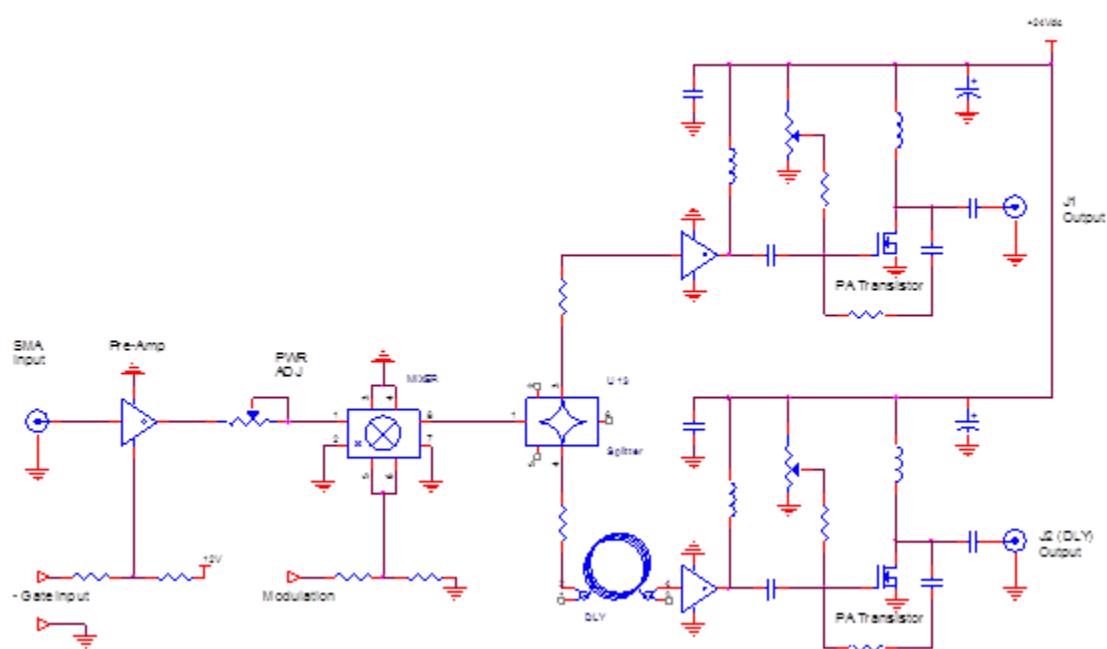


Figure 2: Driver Block Diagram

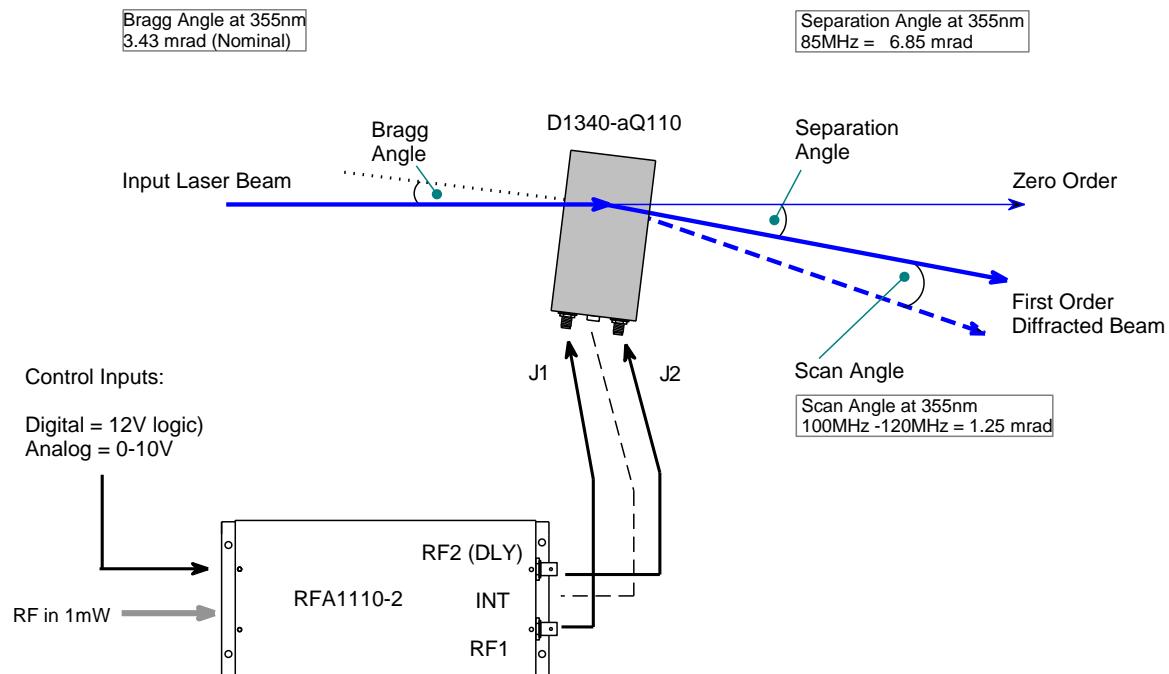


Figure 4: Typical Connection Configuration

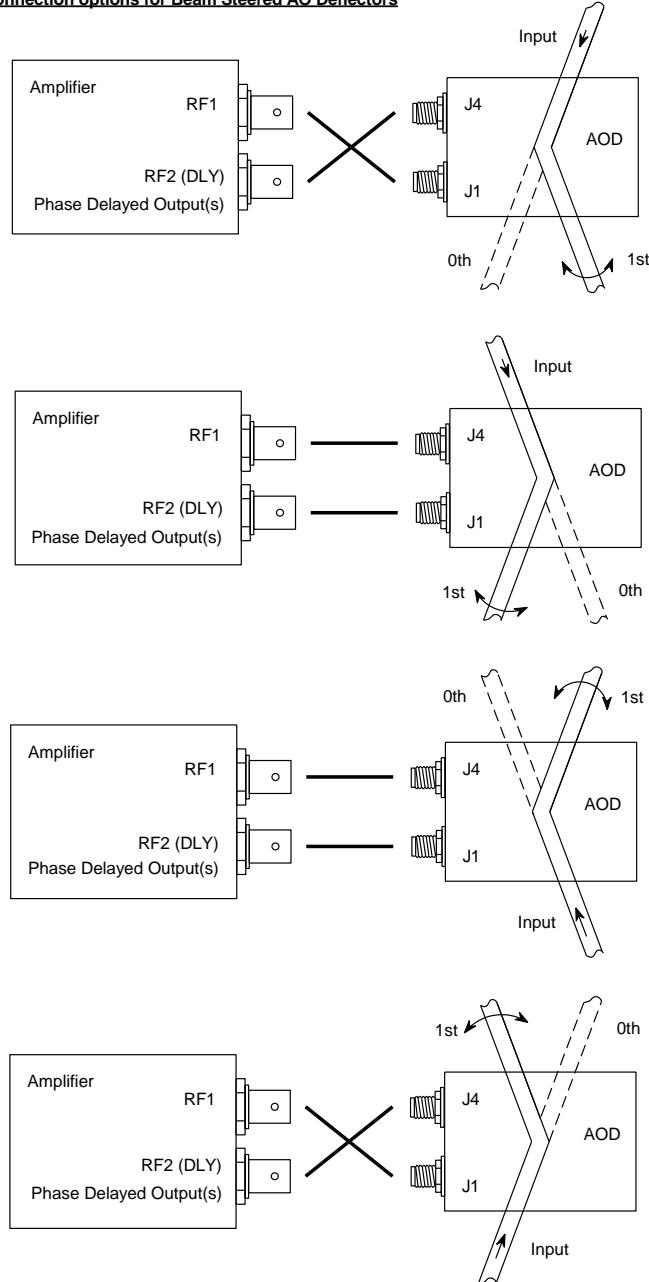
Diagram shows typical beam alignment.

Laser can be input either side of AOM.

See connection options below.

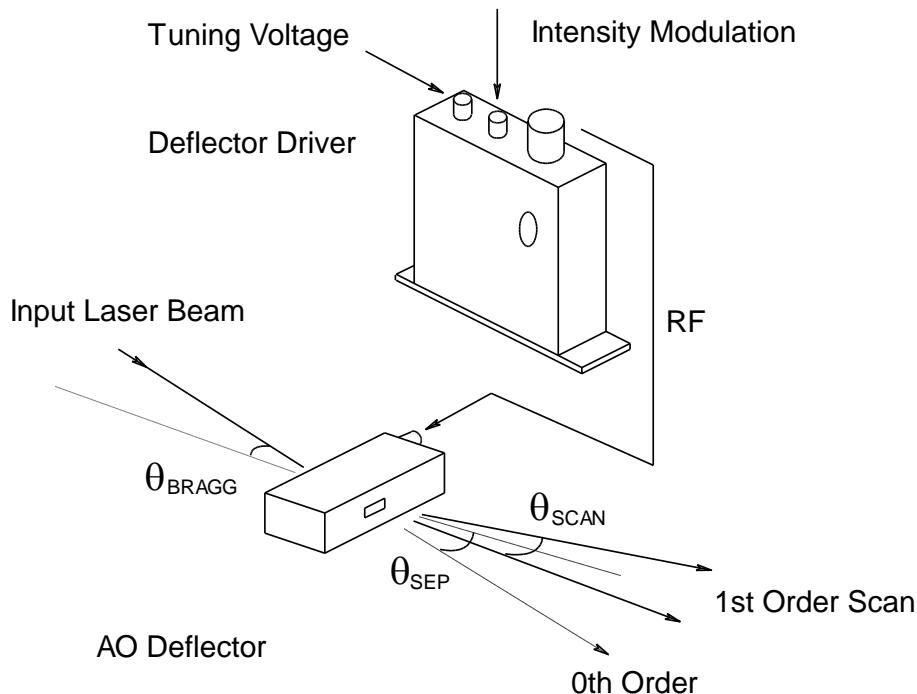
Connection options

Connection options for Beam Steered AO Deflectors



Correct orientation as viewed from top of AOD
(Connector identification may differ)

Schematic of a single electrode acousto optic deflector and tunable driver



The input Bragg angle, relative to a normal to the optical surface and in the plane of deflection is :

$$\theta_{\text{Bragg}} = \frac{\lambda \cdot f_c}{2 \cdot v}$$

The separation angle between the zeroth order and mid scan point of the first order is :

$$\theta_{\text{SEP}} = \frac{\lambda \cdot f_c}{v}$$

The first order scan angle is :

$$\theta_{\text{SCAN}} = \frac{\lambda \cdot \delta f}{v}$$

where:

λ = wavelength

f_c = centre frequency = 110MHz

v = acoustic velocity of interaction material = 5.7mm/usec (a-Quartz)

$d = 1/e^2$ beam diameter

Figure 5. Deflection System